Final Design Plan Permit Condition E.9(c)

Envirosafe Services of Ohio, Inc.

April 26, 2019 Revised July 25, 2019







#### Leachate Management

Currently ESOI is managing the collected nonhazardous trench water and leachate from the facility at 876 Oregon Road through various disposal options. Trench water that does not meet the on-site NPDES discharge requirements is collected in on-site tanks and then transported off-site by truck. The current primary disposal location is a manhole into the City of Toledo sanitary sewer on Geo. Gradel Company Front Street property.

Nonhazardous SWMU leachate is collected in on-site tanks and then transported off-site by truck. The current primary disposal location is either a manhole into the City of Toledo sanitary sewer on Geo. Gradel Company Front Street property or DART a Clean Earth Company depending on contaminant concentrations.

Leachate and/or Trench water may not always meet sanitary sewer discharge standards so other vendors are utilized as necessary.

While the Preliminary Design submitted in September, 2018 indicated that ESOI is planning to design a direct connection to a publicly available sewer, disposal through into a public sewer utilizing a discharge point close to the facility was included as an alternate management method. For the foreseeable future ESOI intends to continue the management of nonhazardous trench water and leachate by methods describe above. ESOI is reserving future potential to design and construct a direct connection to a sanitary sewer.

#### SWMU 5 LNAPL Removal

Corrective action to be undertaken at SWMU 5 includes the active removal of NAPL from the subsurface. The active system is designed to utilize an active NAPL skimmer system. The skimmer will recover the floating hydrocarbons from two wells using a density float skimmer and oleophilic/hydrophobic filter that differentiates between floating hydrocarbons and water. The skimmer will float just above the oil/water interface to collect and remove the NAPL from the well. The removed NAPL will be stored in a 55 gallon drum at the ground surface. The system will be powered using a solar panel.

The preliminary Design assumed that two new wells would be installed for NAPL removal from SWMU 5. During a meeting on March 7, 2019 with Mannik & Smith and Ohio EPA it was suggested that the existing wells may be acceptable for use with the skimmer. Mannik and Smith has researched this suggestion further and found that the existing wells are of sufficient size to accommodate the skimmer. Wells T-20S(2) and T-20S(5) will be used for NAPL removal. As practical, additional wells can be used for NAPL recovery. The solar sipper system is flexible and the equipment can be moved from well to well.

#### SWMU 6 Northern Sanitary Landfill

The Preliminary Design included a document titled *Excavation Plan for Waste Removal North of the North Sanitary Landfill Fence Line* (Excavation Plan). This document detailed the sequencing, the preparation and the security necessary to relocate the small amount of waste north of the SWMU 6 fence line into Cell M. During a meeting on March 7, 2019, Ohio EPA raised two questions regarding the plan as submitted:

1. Will the waste be loaded into trucks and taken directly to Cell M or will it be stored in roll-offs at the site of excavation?

Section 10 addresses this question. "Excavated solid waste material shall be directly loaded onto dump trucks and transported to Cell M . . . "

2. How will ESOI maintain security during the time that the excavation is taking place?

Section 12 addresses this question. "ESOI will remove the fencing along the impacted area on a daily basis. At the end of each working day, temporary fencing will be installed to maintain security. Upon completion of all work the permanent fence will be reinstalled."

The relocation of waste is intended to be accomplished in accordance with the Excavation Plan as submitted with this Class 1 modification.

#### SWMU 8 Old Oil Pond

The Corrective Action work to be done for SWMU 8 includes:

- Installation of a sheet pile wall around the entire waste management unit
- Cap enhancement including grading to promote surface water drainage off of the waste management unit
- Landfill gas venting, and
- NAPL recovery wells
- Demolition of Building C
- Closure of Butz Crock and the Building C heating oil tank
- Improvements to the storm water ditches and AOC 1 (Toledo Waterline Easement)

Currently there is no evidence of contaminants leaking from SWMU 8. The groundwater wells monitoring the waste management unit have not shown any impacts. The corrective action chosen for this unit is intended to mitigate the occurrence of oily seeps at the surface. One of the main causes for the seeps is believed to the buildup of gas pressure. As the pressure increases, it is pushing the oily materials to the surface. Installing gas vents will relieve the pressure and decrease the driving force for the seeps. Additionally, recovering some of the NAPL from SWMU 8 will mitigate the seeps by reducing the source. The sheet pile wall will be installed to accentuate the existing low permeability soils. Sheet pile will be installed below ground surface and keyed into the existing upper till clay unit.

The cap enhancement is intended to ensure positive drainage off of the waste unit. SWMU 8 will be divided into two areas for the management of surface water. The eastern section that is at a higher elevation will be graded such that surface water is conveyed to the northeast corner and ultimately to the pond east of Cell I. The western section, where Building C sits, will be graded such that surface water flows generally to the north and west into the ditch to the south of the waterline easement. As part of the grading work, Building C will be demolished. ESOI intends to leave the concrete slab in place and will place 1.5 to 2 feet of soil over the slab.

Butz Crock, the heating oil tank and associated utilities and any other units encountered within SWMU 8 such as the septic tank associated with AOC 4, the two waste water tanks associated with AOC 5, the second utility vault, will be abandoned in place. Any liquid present in these structures will be removed. A flowable fill will then be used to fill the structure in a manner that will minimize subsidence and prevent additional liquid from collecting. Butz Crock and associated utilities may be removed if in place abandonment interferes with installation of the sheet pile wall.

Improvements to the surface water ditches to the north and south of the City of Toledo Waterline Easement between SWMUs 8 and 9 will consist of regrading to promote drainage and lining with a geosynthetic to minimize infiltration. The waterline easement will also be assessed to determine if there is a need to regrade the soil over the waterline to ensure that surface water is shed to the ditches on the north and south and not allowed to pond on top of the easement.

#### SWMU 9 Northern Sanitary Landfill

The Corrective Action work to be done for SWMU 9 includes:

- Installation of a composite cap
- Final grading that promotes the flow of surface water off of the SWMU

Currently SWMU 9 has a large depression on top of the unit that collects surface water. This surface water is seeping through the existing cap into the waste below and eventually pushing out the sides as leachate outbreaks. The initial work to be done for SWMU 9 corrective action will be to investigate the condition of the existing subgrade. This investigation will determine how much, if any, subgrade needs to be removed and reconstructed before the composite cap can be installed. In addition to reconstructing subgrade as necessary, SWMU 9 will be graded to remove any depressions so that surface water will not collect on top of the composite cap.

The composite cap is to be installed as shown on the attached plan sheets. Surface water will be directed to the existing channels and ponds. The composite cap will include a drainage layer to promote the removal of water from the cap system and direct it into the existing channels.





## SWMU 5 LNAPL



#### 1.1 Basis of Design

The purpose of this design analysis is to develop plans to recover NAPL from the area on the west side of SWMU 5 identified during the RFI field investigation. By removing the NAPL the potential for an unacceptable human health risk due to surface seepage will be eliminated. Alternative designs for the removal of NAPL were developed considering the existing conditions of SWMU 5; the design process considered the following design criteria:

#### • Removal of NAPL from the west side of SWMU 5 to the extent practicable

During RFI field investigation, subsurface NAPL was recovered from monitoring wells installed into a peat layer along the west side of SWMU 5. A summary of the NAPL measurements and characterization of this liquid is provided in Appendix G. The presence of this material was determined to present a potentially unacceptable human health risk to outdoor routine facility workers if surficial seepage of this material occurred. It was noted in the RFI that the NAPL is from off-site/upstream releases to Otter Creek that occurred prior to construction of the perimeter soil berm for SWMU 5. Nonetheless, ESOI is addressing the presence of NAPL on the facility as part of its corrective measures program.

#### 1.2 Development of Design

#### Remove NAPL to the extent practicable with a solar powered active recovery system

The CMS Report discusses use of a passive system and an active system for the recovery of NAPL in the wells on the west side of SWMU 5. The active system is the chosen corrective measure because it is the more efficient process to remove the NAPL.

The active system is designed to utilize an active NAPL skimmer system. The skimmer will recover the floating hydrocarbons from two wells using a density float skimmer and oleophilic/hydrophobic filter that differentiates between floating hydrocarbons and water. The skimmer will float just above the oil/water interface to collect and remove the NAPL from the well. The removed NAPL will be stored in a 55 gallon drum at the ground surface. The system will be powered using a solar panel. Additional system information regarding the solar sipper system can be found in the attached manufacturer cut sheets.

Wells T-20S(2) and T-20S(5) will initially be utilized for NAPL removal. These wells had the most consistent presence of NAPL present during the LNAPL monitoring that took place from July 2006 through November 2007 as documented in the CMS Report. In T-20S(2) the depth to NAPL was between 13.97 and 15.98 feet and the thickness of the NAPL layer ranged from 0.06 to 0.01 feet. In T-20S(5) the depth to NAPL was between 4.80 and 6.87 feet and the thickness of the NAPL layer ranged from 2.41 to 0.01 feet. Well logs for T-20S (2) and T-20S(5) are attached. As practical, additional wells can be used for NAPL

recovery. The solar sipper system is flexible and the equipment can be moved from well to well.

It is anticipated the control panel, solar array, battery and recovery tank will be located within the ESOI fence line to provide security to these components. Manufacturer's data for the Solar Sippers indicates they can operate to depths up to 180 feet, which allows the location of the control and solar array to be situated at a location that maximizes solar exposure. The collection drum, controller and solar array are anticipated to be installed near the top of SWMU 5 where there is no tall vegetation to block the solar panels and where there is access for equipment to maneuver when the collection drum needs to be emptied. One controller will be able to operate both Solar Sippers to collect material from each of the recovery wells. The Solar Sippers will be operated during the time of year without prolonged periods where temperatures are below freezing; typically from April 1 to November 1.

During the active recovery period, LNAPL monitoring will continue at four wells (T-20S[2], T-20S[5], T-20S[7] and T-20S[8]) in the area. Once recovery using this system reaches practical limits (Geotech Solar Sipper operational information indicate the Sippers can skim the LNAPL down to a sheen), adsorbent socks will be used to address any measurable NAPL that continues to accumulate in the well(s).

FIGURES



Well	Oil in Voids/Staining	Interval (feet bgs)	Peat/Organic Layer/Staining	Peat/Organic layer depth (ft)	Well Screen Depth (ft)	NAPL in Well	Notes						
							*Soil description from 0 -	23 feet bgs					
							based on drill cuttings an	d field					
TLW-1	No oil noted		Peat	21 -23	6 - 21	ND	observations.						
T-19W	No oil noted		Peat	15 - 18	10 - 15	ND							
	Staining	18 - 22	Staining/Organics	6 - 9									
T-20W	No oil noted				9 - 14	ND	*Soil description taken fro	om T-20S					
T-20S	Staining	14 - 16	Peat	16 - 18	17 - 22	ND							
	Oil in voids/staining	18 - 19											
	Staining	19 - 22											
T-20S(1)	Staining/odor	6 - 7	Staining/Organics	6 - 7	9.5 - 14.5	ND							
	Staining	8 - 9.5, 10.3 - 10.5											
T-20S(2)	Staining	11.6 - 17	Peat	18 - 20	16 - 21	Yes							
	Oil in voids	14.2 - 14.5, 17 - 18	Staining/Organics	14 - 18									
	Odor	12 - 18, 19 - 20											
T-20S(3)	Oil in voids/odor	6.3 - 6.8	Peat-like material	3.8 - 4, 7.5 - 8	8.5 - 13.5	ND							
	Staining	10 - 10.5											
T-20S(4)	Staining	6 - 9.9, 14 - 16	Peat-like Material	5.8 - 6.1	13 - 18	ND							
	Oil in voids	9.5 - 9.9, 12 - 14	Peat	9.9 - 12									
	Odor	11.9 - 14											
T-20S(5)	Oil in voids	4 - 6.8	Peat	5.8 - 10	7 - 12	Yes							
	Odor	4 - 8											
T-20S(6)	Odor	10 - 12	Peat-like material	14 - 16	16 - 21	ND							
	Oil in voids	17 - 18, 19 - 19.6, 20.4 - 21.5											
	Staining	10.5 - 14, 17 - 18											
T-21S	No oil noted		Peat-like Material	16 - 20	17 - 22	ND							
	Staining	15 - 15.5											
T-21D	Odor	15 - 16.5, 18.75 - 20.75	Peat	16.5 - 17	63 - 68	ND							
T-22W	Staining	9.5 - 12	Peat-like material	9.5 - 12	7 - 12	ND	*Soil description taken fro	om T-22S					
	No oil noted												
T-22S	Staining	9.5 - 12	Peat-like material	9.5 - 12	16 - 21	ND							
	No oil noted		Peat	12 - 15.5									
T-22D	Odor	9 - 11	30% Peat	11 - 15	56 - 61	ND							
	No oil noted		Peat-like Material	15 - 16									
T-45W	No oil noted				8 - 13	ND							
	Staining	10 - 15											
T-46W	No oil noted				7 - 12	ND							
	Staining	7 - 8											
T-47W	No oil noted		Peat	8.5 - 9.5, 12 - 12.5, 14 - 16	11 - 16	ND							
	Staining	4.5 - 6.5, 9.5 - 12											
MR-3D	No oil noted				63 - 68	ND							



Note: Strata to the west of T-20S(5) are estimated, as no borings were conducted west of this location.



	-	
DATE	DRWN	REVISIONS





TABLES

	Table 3a LNABL Maniferring													
				LNAPL Mor	itoring									
				ESOI Otter Cre	ek Facility									
				Oregon, (	Dhio									
				Millard Road Land	Ifill SWMU 5									
Date	Well	Depth to NAPL (ft)	Depth to Water (ft)	LNAPL Thickness (ft)	Comments									
7/20/2006	T-20S(1)		4.97		Wells were checked for DNAPL. No DNAPL was present									
7/20/2006	T-20S(2)	13.97	14.00	0.03	Wells were checked for DNAPL. No DNAPL was present									
7/20/2006	T-20S (3)		6.17		Wells were checked for DNAPL. No DNAPL was present									
7/20/2006	T-20S (4)		10.19		Wells were checked for DNAPL. No DNAPL was present									
7/20/2006	T-20S (5)	6.55	7.53	0.98	Wells were checked for DNAPL. No DNAPL was present									
7/20/2006	T-20S (6)		13.99		Wells were checked for DNAPL. No DNAPL was present									
7/20/2006	MR-6S		12.88		Wells were checked for DNAPL. No DNAPL was present									
7/20/2006	T-21S		15.44		Wells were checked for DNAPL. No DNAPL was present									
7/20/2006	TLW-1		11.83		Wells were checked for DNAPL. No DNAPL was present									
	-	-	-											
7/25/2006	T-20S (2)	14.24	14.28	0.04										
7/25/2006	T-20S (5)	6.7	7.71	1.01	Sampled on July 25, 2006, effectively removing the NAPL layer									
7/26/2006	T-20S (1)		5.3											
7/26/2006	T-20S (2)	14.22	14.25	0.03										
7/26/2006	T-20S (3)		6.42											
7/26/2006	T-20S (4)		10.4											
7/26/2006	T-20S (5)	6.83	7.12	0.29										
7/26/2006	T-20S (6)		14.12											
7/27/2000	T 200 (5)	674	7.00	0.26										
//2//2006	1-208 (5)	0.74	7.00	0.20										
7/28/2006	T-208 (5)	5 59	5 70	0.20	Heavy rain fall the previous night									
//28/2000	1-205 (5)	5.57	5.17	0.20	neavy rain ten the previous night									
8/1/2006	T-20S (1)	I	5 16											
8/1/2006	T-20S(2)	14.1	14.13	0.03										
8/1/2006	T-20S (3)		6.22											
8/1/2006	T-20S (4)		10.3											
8/1/2006	T-20S (5)	6.34	6.63	0.29										
8/1/2006	T-20S (6)		13.98											
8/1/2006	MR-6S		13.06											
8/1/2006	T-20W		8.54											
8/1/2006	T-21S		15.46											
8/1/2006	T-46W		10.31											
8/1/2006	T-47W		14.19											
8/1/2006	T-45W		11.11											
8/1/2006	TLW-1		12.25											
	I	T												
8/3/2006	T-20S (1)		5.14											
8/3/2006	T-20S (2)	14.08	14.09	0.01										
8/3/2006	T-20S (3)		6.21											
8/3/2006	T-20S (4)		10.31											
8/3/2006	1-205 (5) T 205 (C)	6.53	6./l	0.18	Checked for DNAPL, but it was not present.									
8/3/2006	1-203 (0) MD 69		14.03											
0/3/2000 8/2/2004	T 20W		0 51											
8/3/2006	T_21S		0.31 15 51											
8/3/2000	T-46W		10.24											
8/3/2000	T-40W		10.34											
8/3/2000	T-45W		14.14											
8/3/2000	TLW-1		12 30		Checked for DNAPL, but it was not present									
0/0/2000			12.57		cheened for Dinning, out it mus not probent.									

	Table 3a LNAPL Monitoring ESOI Otter Creek Facility Oregon, Ohio Millard Road Landfill SWMU 5													
				Millard Road Land	dfill SWMU 5									
10/26/2006	T-47W		14.32											
10/26/2006	T-45W		10.37											
10/20/2006	<b>T 0</b> 0 <b>C</b> (1)													
10/30/2006	T-20S(1)		5.54											
10/30/2006	T = 20S(2)	14.4	14.41	0.01										
10/30/2006	T - 20S(3) T 20S(4)		10.15											
10/30/2006	T-205 (4)	6.27	6.28	0.01										
10/30/2006	T-20S (6)		13.78											
10/30/2006	T-20S (7)		7.4		DTB from TOC is 17.47'									
10/30/2006	T-20S (8)		13.37		DTB from TOC is 20.33'									
10/30/2006	MR-6S		13.19											
10/30/2006	T-20W		8.23											
10/30/2006	T-21S		14.8											
10/30/2006	T-46W		10.54											
10/30/2006	T-47W		13.19											
10/30/2006	T-45W		10.37											
10/30/2006	TLW-1		10.37		m) (001									
11/1/2006	T-20S(1)		5.67		Time: 1301									
11/1/2006	T-20S (2)	14.56	14.57	0.01	Time: 1312									
11/1/2006	1-20S (3)		0.18		Time: 1259									
11/1/2006	T-205 (4)		6 25		Time: 1209									
11/1/2006	T-205 (5)	0.15	13.94	0.2	Time: 1253									
11/1/2006	T-20S(0) T-20S(7)		7.5		Time: 1306									
11/1/2006	T-20S(8)		11.94		Time: 1303									
	( - )													
8/27/2007	T-20S (1)		5.72		Wells were checked for DNAPL. No DNAPL was present									
8/27/2007	T-20S (2)	15.39	15.45	0.06	Wells were checked for DNAPL. No DNAPL was present									
8/27/2007	T-20S (3)		6.33		Wells were checked for DNAPL. No DNAPL was present									
8/27/2007	T-20S (4)		10.41		Wells were checked for DNAPL. No DNAPL was present									
8/27/2007	T-20S (5)	6.62	6.86	0.24	Wells were checked for DNAPL. No DNAPL was present									
8/27/2007	T-20S (6)	14.94	14.95	0.01	Wells were checked for DNAPL. No DNAPL was present									
8/27/2007	T-20S (7)		7.69		Wells were checked for DNAPL. No DNAPL was present									
8/27/2007	T-20S (8)		10.26		Wells were checked for DNAPL. No DNAPL was present									
8/27/2007	MK-05 T 215	14.72	14.73	0.01	Wells were checked for DNAPL. No DNAPL was present									
8/27/2007	1-215 TI W_1		13.12		Well is missing, presumed destroyed									
8/2//2007	11.00-1				wen is missing, presumed destroyed.									
				SWMU 5 LNAPL F	Bail-down Test									
					Time: 1720 No FP or sheen noted on purged water, will not include in									
8/27/2007	MR-6S	14.72	14.73	0.01	bail-down test.									
8/27/2007	T-20S (2)	15.42	15.45	0.03	Time: 1725									
8/27/2007	T-20S (5)	6.62	6.86	0.24	Time: 1748									
8/27/2007	T-20S (6)	14.96	14.97	0.01	Time: 1740									
8/27/2007	T-20S (2)	15.98	15.99	0.01	Time: 1800									
8/27/2007	T-20S (5)	6.8	6.84	0.04	Time: 1752									
8/27/2007	T-20S (6)	15.3	15.31	0.01	Time: 1807									
	<b>T A C C C</b>		<b>2</b>	-	T. 1000									
8/27/2007	T-20S (2)	15.96	15.97	0.01	Time: 1830									
8/27/2007	T-20S (5)	6.68	6.72	0.04	11me: 1812									
8/27/2007	1-208 (6)	15.32	15.33	0.01	11me: 1821									

	Table 3a LNAPL Monitoring ESOI Otter Creek Facility Oregon, Ohio Millard Bood L andfill SWMU 5													
				Millard Road Land	Ifill SWMU 5									
0 (0 ( <b>0</b> 0 0 d														
8/8/2006	T-20S (1)		5.49											
8/8/2006	T-20S (2)	14.38	14.395	0.015	Checked for DNAPL, but it was not present.									
8/8/2006	T = 20S(3)		0.40											
8/8/2006	$T_{-20S}(4)$	6.83	10.J	0.03	Checked for DNAPL but it was not present									
8/8/2006	T-205 (5)	0.05	14 22	0.05	checked for DIVALE, but it was not present.									
8/8/2006	MR-6S		13.19											
8/8/2006	T-20W		8.83											
8/8/2006	T-21S		15.61											
8/8/2006	T-46W		10.53											
8/8/2006	T-47W		14.49											
8/8/2006	T-45W		11.97											
8/8/2006	TLW-1		12.91											
0/10/200	<b>T 0</b> 00 (1)		1											
8/10/2006	T-20S (1)		5.38											
8/10/2006	1-20S(2) T 20S(2)	14.31	14.32	0.01	Checked for DNAPL, but it was not present.									
8/10/2006	$T_{-20S}(3)$ $T_{-20S}(4)$		10.44											
8/10/2006	$T_{-20S}(4)$	6.87	6.89	0.02	Checked for DNAPL but it was not present									
8/10/2006	T-20S (6)		14 19		checked for Diffit E, but it was not present.									
8/10/2006	MR-6S		13.24											
8/10/2006	T-20W		8.87											
8/10/2006	T-21S		15.6											
8/10/2006	T-46W		10.54											
8/10/2006	T-47W		14.41											
8/10/2006	T-45W		12.02											
8/10/2006	TLW-1		12.81											
10/24/2006	T 200 (1)		5.26											
10/24/2006	1-20S(1)		5.26											
10/24/2006	$T_{205}(2)$ $T_{205}(3)$	14.14	6.13	0.01										
10/24/2006	T-20S(3) T-20S(4)		10.22											
10/24/2006	T-20S (5)	6.15	8.56	2.41	Bailed down NAPL									
10/24/2006	T-20S (6)		14.02											
10/24/2006	MR-6S		13.17											
10/24/2006	T-20W		8.52											
10/24/2006	T-21S		15.08											
10/24/2006	T-46W		10.98											
10/24/2006	T-47W		14.1											
10/24/2006	T-45W		10.37											
10/24/2006	ILW-I		10.87											
10/26/2006	T_20S (1)		6 27											
10/26/2006	$T_{-20S}(1)$	15 27	15.28											
10/26/2006	T-20S(2) T-20S(3)	1.5.27	6 33											
10/26/2006	T-20S (4)		10.64											
10/26/2006	T-20S (5)	6.74	6.78	0.04										
10/26/2006	T-20S (6)		14.14											
10/26/2006	MR-6S		13.25											
10/26/2006	T-20W		8.51											
10/26/2006	T-21S		15.33											
10/26/2006	T-46W		10.76											

Table 3a LNAPL Monitoring ESOI Otter Creek Facility Oregon, Ohio <u>Millard Road Landfill SWMU 5</u>													
11/28/2007 T-20S (1) 6.5 Wells were checked for DNAPL. No DNAPL was present													
11/28/2007 T-20S (2)	14.92	15.30	0.38	Wells were checked for DNAPL. No DNAPL was present									
11/28/2007 T-20S (3)		7.27		Wells were checked for DNAPL. No DNAPL was present									
11/28/2007 T-20S (4)		11.10		Wells were checked for DNAPL. No DNAPL was present									
11/28/2007 T-20S (5)	4.80	6.50	1.70	Wells were checked for DNAPL. No DNAPL was present									
11/28/2007 T-20S (6)	15.80	16.20	0.40	Wells were checked for DNAPL. No DNAPL was present									
11/28/2007 T-20S (7)		7.80		Wells were checked for DNAPL. No DNAPL was present									
11/28/2007 T-20S (8)		11.90		Wells were checked for DNAPL. No DNAPL was present									

	Table 3a LNAPL Monitoring ESOI Otter Creek Facility Oregon, Ohio Millard Road Landfill - SWMU 5														
	Ate Well NAPL (ft) Water (ft) Thickness (ft) Comments														
Date	Well	NAPL (ft)	Water (ft)	Thickness (ft)	Comments										
	T-20S (1)		5.53		Wells were checked for DNAPL. No DNAPL was present										
	T-20S (2)	15.5	15.83	0.33											
	T-20S (3)		5.95		Wells were checked for DNAPL. No DNAPL was present										
	T-20S (4)		10.11		Wells were checked for DNAPL. No DNAPL was present										
	T-20S (5)	6.06	6.79	0.73											
	T-20S (6)	14.93	15.09	0.16											
6/2/2010	T-20S (7)		7.46		Wells were checked for DNAPL. No DNAPL was present										
	T-20S (8)		11.95		Wells were checked for DNAPL. No DNAPL was present										
	MR-6S		14.76												
	T21S		15.36		Wells were checked for DNAPL. No DNAPL was present										
	T20W		8.18		Well is missing, presumed destroyed.										
	T45W		12.15												
	T46W				Unable to locate, presumed abandoned.										

### Hydrocarbon Recovery System

### Geotech Single & Multi-Well Solar Sipper

The Geotech Solar Sipper is a solar powered remediation system, designed for remote applications where electrical power is either not available or not economically feasible. This uniquely flexible system can be configured for up to eight wells. The compact, easy to install features make this unit efficient to move and implement multiple wells.

The Solar Sipper uses a unique downwell pump to recover hydrocarbons through a floating oleophilic/hydrophobic intake filter. Once the pump canister is filled via the vacuum cycle, the pump reverses, pressurizes the system and pumps the recovered fluid to the surface and into a storage vessel.

The Geotech Solar Sipper can effectively extract fluids from depths to 180 feet below ground surface and recover viscous hydrocarbons such as 90 weight oil when our heavy oil skimmer is utilized.

#### **EASE OF DEPLOYMENT**

The Solar Sipper can reduce overall project costs and dramatically improve deployment:

- Available in single or multi-well configurations
- Reduces the time and cost for a power line to be run to a site.
- · Eliminates the need for electricians to do install work and permitting.
- The simple and safe low voltage system can be installed without special training or licensing and requires minimal experience.
- No trenching or transformer equipment is required.
- Relocating equipment to follow a plume or to adjust to new site characterization information is fast and easy.

#### **OPERATION**

The Geotech Solar Sipper recovers floating hydrocarbons (LNAPL) from wells using a solar powered pressure/vacuum pump. The standard Skimmer features a unique product intake assembly that incorporates both a density float and an oleophilic/hydrophobic filter that differentiates between floating hydrocarbons and water. The skimmer floats just above the oil/water interface to collect and remove hydrocarbons from the well into an optional above ground storage tank.

The Geotech Solar Sipper is also available for recovery of sinking product (DNAPL) from wells when using a fixed intake.





Control Panel and Pressure/Vacuum Pump (eight-well controller shown)



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## Hydrocarbon Recovery System

# geotech

### Geotech Single & Multi-Well Solar Sipper

#### **DESIGN YOUR RECOVERY SYSTEM**

#### **Step 1: Control Panel**

- Choose from 1 to 8 wells
  - NEMA 3R Enclosure
  - Tankfull Shut-Off Switch (<sup>3</sup>/<sub>4</sub>" or 2" NPT bung-fitting)
  - Microprocessor Controlled 2-Line LCD Display with four scroll buttons
  - On/Off Switch
  - Pressure/Vacuum Pump
  - Pressure/Vacuum Gauge

#### **Step 2: Solar Accessories**

- ✓ 100 watt solar panel(s) with adjustable mounting frame
- ✓ AGM Solar Batteries 104 AH, 12 Volt

#### AC powered versions are available



#### **Step 3: Downwell Equipment**

- ✓ Downwell Pump(s)
  - Standard
  - With Conductivity Sensor
- Skimmer(s)
  - 2" or 4" Skimmer with 100 or 60 Mesh Intake
  - 2" or 4" Protective Screen
  - 4" Skimmer with Extended Travel
  - 4" Heavy Oil Skimmer
  - 4" High Temperature/Heavy Oil Skimmer
  - 2" DNAPL Intake

#### **Other Options:**

- 2" or 4" Slip Fit Well Cap(s)
- Choose Length: Air and Discharge Tubing
- ✓ 55 Gallon Steel Product Drum(s)
- Dual-Wall Containment Product Recovery Tank(s)
- Lockable Weatherproof Enclosure
- Trailer for Mounting Mobile System
- Telemetry Packages



3-Well Solar Sipper on trailer with dual containment tank



Solar Sipper installation with bovine protection



Solar Sipper installation mounted on hazmat enclosure

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### Hydrocarbon Recovery System

## geotech

### Geotech Single & Multi-Well Solar Sipper

#### **SPECIFICATIONS**

Applications:	2" (50 mm) or larger recovery wells									
<b>Recovery Rate:</b>	.2 gallons (757 ml) per cyc	le								
Maximum Operating Depth:	180 feet (55m)									
Power Requirements:	12-15 Volts DC input @ up 90~240 Watts continuous	o to 14.5 Amps								
Maximum Pressure:	100 PSIG (7 bar)									
Maximum Vacuum:	20" Hg @ MSL (50mm Hg)									
Oil/Water Separation:	Oleophilic/hydrophobic r	nesh screen								
Controller: Operating Temperature Storage Temperature Range Humidity Size	32° to 104°F (0° to 40°C) -20° to 150°F (-29° to 66°C 90% non-condensing (ma 10" D x 18" T x 16" W (25.4	.) ax) Icm D x 45.7cm T x 40.6cm W)								
Rating	49 lbs. (22. 2 kg) eight channel NEMA 3R									
Optional Solar Panel w/Frame: Rated Power Operating Voltage Maximum Voltage Operating Amperage Maximum Amperage Size Approximate Weight Optional Downwell Pump: Size	100 Watts (standard unit) 17.4 Volts DC 21.5 Volts DC 4.88 Amps (standard unit) 5.8 Amps 41.2" H x 27.5" W (105 cm H x 70 cm W) 23.3 lbs. (10.5 kg)									
Weight Materials	4.5 lbs. (2.04 kg) 303 and 304 Stainless Ste	el, Flexible Rubber Tubing, PVC, Brass								
Optional Skimmer Assemblies: Effective Travel Range Size Weight Operating Temperature Storage Temperature Materials	2" Model      4" Model        12" (30.5cm)      24" (61 cm)        35.5" L x 1.75" OD      35.5" L x 3.75" OD        (90.2cm L x 4.4cm OD)      (90.2cm L x 9.5cm OD)        1.75 lbs. (.79 kg)      2.25 lbs. (1.02 kg)        32° to 104°F (0° to 40°C)      -        -20° to 150°F (-29° to 66°C)      304 Stainless Steel, Polyethylene, PVC, Polypropylene, Bras									
<b>Optional Tubing:</b> Air Discharge	.17" ID (4.3mm ID) .375" ID (9.5mm ID)									

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		r. 1940			<b>Page</b> 1 of 2	Temporary Mo	nitoring	Well	Nur	nbe	er: 1	<b>-20</b> S	(2)						
()	Mannik Project No: F200 Project Name: En Client: ESOI Oreg Site Location: SV Construction Ma	Group Group TQ2 TQ2 gon F WMU	safe SW acility 5 chedule	<b>111</b> 7MU5 F 40 PV	MSG Perso Approved I Contractor Driller: Ton Drilling Me Drill Rig: C Screen Slo	MSG Personnel: Nicholas Bohland Approved By: Contractor: TTL Associates, Inc. Driller: Tony Brister Drilling Method: 4.25 HSA w/ SS Drill Rig: CME 550 ATV Screen Slot Size: 0.010 inch					Boring Depth: 24 feet Northing: 11540.72 Easting: 9748.97 Top of PVC Elev.: 589.70 feet Ground Surface Elev.: 587.65 feet Pro-casing Mat.: Schedule 40 PVC								
	Riser Length: 18 Screen Length: 5	.05 fe 5 feet	et		Rock Borel	hole Dia.: Not Enco	untered	Filter	Pacl	k Má	n ⊏ at.: #	5 Silic	a Sand						
				S	UBSURFACE	E PROFILE			S	AM	PLI	E DA	ΤΑ						
	Well Construction Details	Depth	Elevation	Symbol		Description		Number	Type	Blows/ft	Recovery	FID/PID (ppm)	Remarks						
	Concrete PVC Riser	Bu -3- -3- -3- -3- -3- -3- -3- -3- -3- -3-				Fround Surface Silty Clay ty Clay with rootlets, som dry. Some black and gra Gravel piece at 4.6 feet.	ne gravel, Ny sand at	SS1 SS2 SS3	SS SS SS	2357 68108 2444	20" 18" 16"	2.9 2.2 1.9							
	ntonite Grout	6 7 7 8	581.65 579.65		Brown and gray Silt depth, stiff to softer orange silt seams.	Silty Clay ty Clay becoming more g with depth, some gravel	ray with and	SS4	SS	4655	20"	2.1							
	Be	9 10	577.65	H H	Gray Silty Clay with feet, dry, stiff. Softe 8.5-10 feet.	some olive-green staini r, damp, and high plastic	ng at 9.2 city from	SS5	SS	2 3 4 2	20"	2.2							
		11 11 12	575.65	HH	Gray Silty Clay with black staining and c feet, moist from 10. plasticity from 10.8-	Slity Clay a some tan and olive-gree blive-green mottles from 5-10.8 feet, damp and m 12 feet.	en mottles, 11.6-12 edium	SS6	SS	4 5 5 5	24"	2.8							
C		13.1	573.65	HH	Gray Silty Clay with throughout, soft, da 13.6 feet, low plasti	Silty Clay olive-green and black si mp, some fine sand (>1r city with a petroleum odo	taining nm) at or.	SS7	SS	0 0 3 4	24"	64.5							
	Bentonite Pel	15_ 16_	571.65	HH	Gray Silty Clay with material, damp, soft small oil spots in vo green staining and s 15 feet.	Silty Clay black staining and organ t, slight petroleum odor, s bids from 14.2-14.5 feet, some wood fragments fro	nic some plive- pm 14.5-	SS8	SS	4 2 2 3	24"	27.9							



	- pro-	њ			<b>Page</b> 1 of 1	Temporary Monitorin	ng Well	l Nu	mbo	er:	T-20S	S(5)
	Mannik Project No: F200 Project Name: En Client: ESOI Ore Site Location: SN Construction Ma	Grou Grou D7Q2 nviro gon F WMU	p, Inc. safe SW acility 5 chedule	<b>nit</b> vmu5	MSG Perso Approved Contractor Driller: Tor Drilling Me Drill Rig: C C Screen Slo	<i>bnnel:</i> Nicholas Bohland <i>By:</i> <i>:</i> TTL Associates, Inc. by Brister <i>thod:</i> 4.25 HSA w/ SS ME 550 ATV <i>t Size:</i> 0.010 inch	Start Borii Norti East Top Grou	/End ng De hing: ing: 9 of PV und S casin	Dat pth 115 741 CE urfa g M	e: 5/ : 14 :98.4 .35 lev.: ce E	/27/04 feet 8 580.5 <b>Elev.:</b>	56 feet 578.33 feet ule 40 PVC
	Riser Length: 9.2 Screen Length: 5	23 fee 5 feet	et		Rock Bore	Rock Borehole Dia.: 8.25 Inch					\$ent. 0 \$5 Silic	a Sand
				S	UBSURFACE	E PROFILE		S	AM	IPL	E DA	ТА
	Well Construction Details	Depth	Elevation	Symbol		Description	Number	Type	Blows/ft	Recovery	FID/PID (ppm)	Remarks
	PVC Riser	-3 -2 -1 -1	578.33	H	G Brown and gray Sill some rust colored s	round Surface Silty Clay ty Clay, damp, low plasticity, with silt from 2-4 feet.		66	53	10"		
1	Concre	2 2 3 1	574.33	HHH			SS2	ss	6 9 4 5 8 8	10"	0.0	
	le Pellets 7	5 5 6	572.33	HH	Brown and gray Sill Black stained at 5.5 rootlets, and peat-li some brown oil in v	Silty Clay by Clay, with a trace of gravel. i feet with wood fragments, ke material from 5.8-6 feet, damp, oids with petroleum odor.	SS3	ss	2 2 3 4	24"	16.1	
	Bentonii	7	570.33		Black stained Peat- black clay, soft, sor brownish peat-like r fragments, rootlets,	Peat like material with some gray and ne oil from 6-6.8 feet. Becoming naterial, crumbly, damp, wood slight petroleum odor.	SS4	SS	2 2 3 2	24"	7.8	
		9 11 10 10	568.33		Brown Peat-like ma to greenish from 9- and gravel, soft, mo clay, sand and grav	<i>Peat</i> terial with some clay, bluish-gray 10 feet, some rootlets and sand bist to saturated with some silty el from 9.8-10 feet.	SS5	SS	1 1 2 2	24"	4.8	
	Sand	11 - 12 -	566.33	HH	Bluish-green Silty C to gray saturated sa inches thick, then si gravel, damp.	Silty Clay clay approximately 3 inches thick, and and gravel approximately 16 tiff gray silty clay with trace of	SS6	SS	1 2 1 4	20"	1.2	
	#5 Silica	13	564.33	HH	Gray Silty Clay with all gray from 13.8-1	<i>Silty Clay</i> trace of gravel, tan silt seams to 4 feet, damp, stiff.	SS7	SS	3 5 8 12	24"	0.8	
		15   11   15   16   17   17   17   17   17   17   17			Er	nd of Borehole						

## SWMU 6 NORTHERN SANITARY LANDFILL



#### 1.1 Basis of Design

The purpose of this design analysis is to develop a plan to relocate waste currently outside of the fence line along the northern edge of the Northern Sanitary Landfill.

• Relocation of waste identified outside of the ESOI fence line

During the initial RCRA RFI and the subsequent North Sanitary Landfill RFI field investigation, a series of borings were installed to delineate the horizontal and vertical extent of waste that exist outside of the facility fence. Analytical data and visual observations obtained during these investigations indicate that the thickness of the solid waste material encountered varied from less than one (1) foot to twelve (12) feet, with most thicknesses less than two (2) feet.

#### **1.2** Development of Design

• Excavation work plan development and goals

A work plan has been developed that outlines the steps to be taken to remove the waste that is outside the fence line and place it into the active Cell M. The work plan is attached.

Considerations discussed in the work plan include:

- Site Description a discussion of where the waste is located. This includes results from the boring investigations that were completed as well as plan sheets that show the location.
- **Construction Sequence** outlines the steps that will be taken to systematically excavate and relocate the waste material.
- **Site Preparation** any necessary work to be sure the area is ready to be excavated (i.e. survey stakes added, grubbing or other surface prep work)
- **Security** explanation of the steps necessary to maintain restricted access and security on site.
- **Evaluation of Potential Permitting Obligations** discussion of any need for additional permits that should be considered prior to the work commencing
- Soil Erosion and Sediment Control / Stormwater Management a description of the controls to be implemented prior to the work commencing
- Soil Excavation and Excavated Soil Management a discussion on the separation of materials during the excavation. Clean soils are to be stockpiled for later use, waste materials are to be disposed of in Cell M.
- Soil Screening identifies methods to be used during excavation to verify or supplement the findings of the boring investigations.
- Soil Disposal, Staging and Loadout excavated waste will be segeregated and properly disposed in Cell M. Clean soil will be staged for use in site restoration.

- Storm Water Runoff and Leachate Control discusses the potential to • manage storm water or leachate and what precautions are to be taken to ensure
- •
- any such liquids are managed appropriately. **Site Restoration** steps to be taken to ensure that area is properly backfilled and vegetation and storm water flow are re-established. **Quality Assurance and Quality Control** outlines the oversight necessary to ensure the excavation plan is appropriately followed. •

**Excavation Plan for Waste removal** 

### EXCAVATION PLAN FOR WASTE REMOVAL NORTH OF THE NORTH SANITARY LANDFILL (NSL) (SWMU 6) FENCE LINE

#### U.S. EPA I.D. NO. OHD 045 243 706

Submitted By:

Envirosafe Services of Ohio, Inc. Oregon, Ohio

Submitted To:

Ohio EPA

Prepared By:



Hatboro, Pennsylvania



Princeton, New Jersey

Date: September 2018

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#### DRAWINGS

- Drawing 1: Site Layout
- Drawing 2: Excavation Plan
- Drawing 3: Soil Erosion and Sediment Control Plan
- Drawing 4: Soil Erosion and Sediment Control Notes and Details

#### 1. INTRODUCTION

This excavation work plan (work plan) has been prepared by Ramboll US Corporation (Ramboll) and Envirosource Technologies, Inc. on behalf of Envirosafe Services of Ohio, Inc. (ESOI) to address removal of buried solid waste delineated north of the North Sanitary Landfill (NSL) Solid Waste Management Unit (SWMU) 6 fence line and property line (see **Drawings 1 and 2**). The horizontal and vertical extents of this waste were characterized as part of soil boring investigation activities completed during the Initial RCRA (Resource Conservation and Recovery Act) Facility Investigation (RFI) and Supplemental NSL RFI. Analytical data and visual observations obtained during these investigation indicate that the thickness of the solid waste material encountered varied from less than one (1) foot to twelve (12) feet, with most thicknesses less than two (2) feet.

A volume of approximately 200 cubic yards of solid waste material will be excavated from this area and relocated to the on-site active landfill, Cell M, for disposal. Based on the delineation sampling conducted as part of the NSL RFI, approximately 0 to 5 feet of soil cover is present over the layer of solid waste material. These soils will be stockpiled and reused for backfill upon removal of the solid waste. Additional backfill will be provided to restore existing grades, and the area will be regraded and seeded. Based on groundwater monitoring and leachate controls in the adjacent SWMU 6, groundwater is not expected to be encountered during the proposed excavation activities.

This excavation work plan is organized as follows:

- Site Description.
- Construction Sequence.
- Site Health and Safety Plan.
- Site Preparation.
- Evaluation of Potential Permitting Obligations.
- Soil Erosion and Sediment Control / Stormwater Management.
- Soil Excavation and Excavated Soil Management.
- Soil Screening.
- Soil Disposal, Staging and Loadout.
- Storm Water Runoff and Leachate Control.
- Site Restoration.
- Quality Assurance and Quality Control.

#### 2. SITE DESCRIPTION

The North Sanitary Landfill was operated from 1976 through 1981 for disposal of solid waste and is equipped with a gas monitoring system and a leachate collection system that was installed as part of ESOI's presumptive correction action activities. The proposed excavation area encompasses the portion of the waste material that extends north of the NSL and the property line, as shown in **Drawing 2**. This area is bounded by the North Sanitary Landfill (NSL) to the south and the Gradel ditch and the Gradel Landfill (an abandoned landfill) to the north. The Gradel ditch only flows during and following precipitation events towards the west and discharges into Otter Creek downstream of the facility.

#### 3. CONSTRUCTION SEQUENCE

The waste area occupies approximately 830 square feet and is located north of the NSL fence line and property boundary. Prior sampling activities conducted in the RFI has horizontally and vertically delineated the extent of the waste material within the area. These results indicate that the waste material is located at limited intervals between approximately 0 to 12 feet bgs within the excavation area.

Construction activities to remove the identified solid waste and restore the area will take place in the following order:

- Site preparation and identification of the delineated solid waste limits (see **Drawing 2**) using GPS to mark out the limits of excavation.
- Removal of approximately 400 feet of existing fencing within the excavation area as depicted on **Drawing 1**.
- Excavation of the top layer of the existing fill (approximately 3 to 5 feet) by visual segregation from underlying waste material; this cover soil will be stockpiled near the work area for use as backfill/topsoil material.
- Removal of waste material at least to the depths shown on **Drawing 2**. Actual excavation depths and extents will be determined based on field observations as described in **Section 10**.
- Collection of contact water (i.e., stormwater and leachate that may collect within the excavation area) in existing on-site fractionation tanks, as needed, for eventual off-site disposal<sup>1</sup>.
- Waste characterization sampling of excavated soils for profiling of the waste for disposal at the on-site active landfill, Cell M, as required by the existing facility RCRA Part B Permit.
- Transport and disposal of solid waste/soils to Cell M.
- Site restoration (backfilling, compacting, regrading, seeding, reinstallation of fencing, removal of soil erosion and sediment control measures).

Note that it is anticipated that several existing explosive gas punch bar locations may be disturbed during the excavation activities. Restoration will be competed for those required by the Explosive Gas Monitoring Plan.

<sup>&</sup>lt;sup>1</sup> As leachate levels are believed to be maintained below the depth of the excavation, accumulation of water within the excavation is not anticipated. However, the fractionation tanks should be on standby in the event that dewatering is warranted.

#### 4. SITE HEALTH AND SAFETY PLAN

All construction activities shall be conducted in accordance with ESOI's Health and Safety Plan (HASP) that complies with OSHA requirements (40 CFR 1910.120).

#### 5. SITE PREPARATION

Prior to groundbreaking, the delineated solid waste boundary beyond the NSL fence line will be staked via a commercial GPS using the coordinates for the excavation limits as depicted on **Drawing 2**. Minor clearing and grubbing will also be required to access the proposed excavation area.

#### 6. EVALUATION OF POTENTIAL PERMITTING OBLIGATIONS

Based on the location of the excavation area and the nature of the proposed work, Ramboll evaluated the need for wetlands and stormwater discharge permitting. As discussed below, Ramboll has not identified any permitting requirements applicable to the planned activities.

A wetland survey conducted as part of the ecological evaluation during the Phase I activities indicate that the Gradel Ditch and the proposed area of disturbance was not identified as a wetland (ENVIRON and MSG, 2003). Therefore, wetland-related permits will not be required for the proposed excavation work.

The Ohio EPA Construction General Permit for Stormwater Discharges is only required if the proposed area of disturbance for a construction project is greater than one acre. Since the threshold area of disturbance will not be met for the proposed excavation activities, this permit and the development of a Stormwater Pollution Prevention Plan (SWP3) will not be required. Soil erosion and sediment control measures will be implemented in accordance with **Section 7** below and **Drawings 3 and 4**.

#### 7. SOIL EROSION AND SEDIMENT CONTROL / STORMWATER MANAGEMENT

Although construction stormwater discharge permits will not be required for this project, ESOI should, as a best management practice, implement soil erosion and sediment control measures consistent with accepted industry practices and described in the Ohio Department of Natural Resources' Rainwater and Land Development Manual (ODNR, 2006). As shown in **Drawings 3 and 4**, silt fencing will be installed around all active soil remediation, handling and staging areas prior to land disturbance. Upon the completion of all construction activities, these controls will be removed for proper disposal, and the backfilled and compacted area will be stabilized with permanent vegetation. The proposed remedial activities will not alter the site hydrology after site restoration since the excavation area will be restored to the existing grades.

## 8. SOIL EXCAVATION AND EXCAVATED SOIL MANAGEMENT

After the delineated excavation boundaries have been staked, the fence fabric removed, and soil erosion and sediment control measures installed, excavation activities may begin. Excavation shall take place in two phases: (1) removal of the top layer of clean soil and stockpiling of the clean soil in the designated area as shown in **Drawings 2 and 3**, and (2) excavation of solid waste material to the depth and extent as shown in **Drawings 2 and 3**.

All excavated soils will be screened, segregated, and staged as summarized in **Section 9**. As such, these soils will be managed based on: (1) screening observations of soil quality made at the time the soils are exposed and disturbed, and (2) existing analytical results. Excavation shall take place one (1) foot beyond the vertical and horizontal footprint of the observed solid waste based on the soil screening described in **Section 9**.

Unless field observations identify materials that appear contaminated or are present outside the pre-delineated area, post-excavation sampling and sampling of the segregated top soil layer will be unnecessary because prior soil and solid waste sampling results in and near the excavation area did not indicate any exceedances of any applicable screening criteria (ENVIRON, 2008).

#### 9. SOIL SCREENING

Although the vertical and horizontal extents targeted for solid waste removal and the thickness of the topsoil layer to be segregated and reused as backfill were previously characterized, soils exposed during excavation will be screened using field observation as noted below to identify any additional soils that have evidence of potential contamination and therefore require segregation and characterization to determine ultimate disposition. Based on prior investigations performed at the site, however, contaminated materials are not expected.

- <u>Visual Inspection</u>: Soils will be visually inspected for evidence of potential contamination or obvious solid waste materials, particularly the presence of soil staining or free product. ESOI will proceed conservatively with disposal of any stained soil regardless of the actual constituent concentrations identified in those soils.
- <u>Olfactory Screening</u>: Soils will be evaluated for unusual odors. Any soils exhibiting odors shall be segregated for possible waste characterization in accordance with the disposal requirements for Cell M at the discretion of appropriate facility representatives.

During the excavation activities, soils will be screened with a photo-ionization detector (PID) for worker health and safety monitoring purposes. Soils that result in elevated PID readings (sustained readings within the breathing zone of 0.5 ppm above background) shall be segregated for possible further characterization as discussed above. In addition, as part of the worker health and safety monitoring, soils will also be screened for potential explosive gases using a landfill gas meter.

#### 10. SOIL DISPOSAL, STAGING, AND LOADOUT

Excavated material not within the top layer of clean material (see **Section 1**) will be disposed of at the on-site active landfill, Cell M (see **Drawing 1**). Excavated solid waste material shall be directly loaded onto dump trucks and transported to Cell M for waste classification, if required, and disposal. At the discretion of appropriate facility representatives, samples of solid waste materials will be analyzed for waste classification in accordance with the requirements of the facility's RCRA Part B Permit.

Soil staging piles for clean material identified in **Drawing 2** will be covered with a double thickness of 8-mil plastic sheeting. The plastic sheeting covering each soil pile will be secured when the staging area is in active use. The soil piles will also be surrounded by hay bales for erosion control. Alternatively, the clean material may be staged in roll-off containers.

#### 11. STORM WATER RUNOFF AND LEACHATE CONTROL

A recovery well system installed for leachate control has been operational in SWMU 6 since July 1, 2007. Additional piezometers were also installed along the NSL's northern and eastern property lines and on the south slope of the Gradel Landfill to monitor water levels. Based on existing groundwater and leachate levels, the presence of leachate and groundwater is not expected to be a significant.

Contact water (any storm water and leachate that accumulates within the excavation area), if any, shall be managed within the excavation by pumping to an existing on-site fractionation tank for eventual off-site disposal, as needed.

#### 12. SECURITY

ESOI will remove the fencing along the impacted area on a daily basis. At the end of each working day, temporary fencing will be installed to maintain security. Upon completion of all work the permanent fence will be reinstalled.

#### **13. SITE RESTORATION**

ESOI will restore excavation areas through backfilling, compacting, and regrading existing site soils and with clean fill from its clay mine stock pile. The backfill material shall be compacted to a minimum of 95% of the Modified Proctor dry density. Soil vegetation shall be restored over the backfilled area using the specifications outlined on **Drawing 4**.

#### 14. QUALITY ASSURANCE AND QUALITY CONTROL

A designated field engineer shall be present during all earthmoving activities to screen soils, track material handling and disposal, and verify and document that all remedial work (i.e., excavation, regrading, topsoiling, and seeding) are completed in accordance with this excavation plan. Additionally, a field engineer shall track all soils loaded and transported to Cell M and inspect the adequacy of soil erosion and sediment control measures. The field engineer shall also monitor dust levels and record observances in the daily field log.

#### **15. REFERENCES**

- ENVIRON International Corporation (ENVIRON) and Mannik & Smith Group (MSG). 2003. *RFI Phase I Report and Phase II Work Plan.* July.
- ENVIRON International Corporation (ENVIRON). 2008. *Resource Conservation and Recovery Act (RCRA) Facility Investigation Final Report.* February.
- ENVIRON International Corporation (ENVIRON) and Envirosource Technologies, Inc. Revised 2012. *Corrective Measures Study (CMS)*. January. April.
- Midwest Environmental Consultants (MEC). 1997. Draft Final RFI Report, Northern Sanitary Landfill. June.
- Ohio Department of Natural Resources. Division of Soil and Water Resources. "Rainwater and Land Development Manual: Ohio's Standards for Stormwater Management, Land Development and Urban Stream Protection." By John Mathews. Dec. 2006.

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EXCAVATION PLAN FOR WASTE REMOVAL

DRAWINGS



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## SWMU 8 OLD OIL POND



#### 1.1 Basis of Design

The purpose of this design analysis is to develop a plan to manage the conditions identified at SWMU 8, the old oil pond, that require corrective measures. During the RFI it was determined that landfill gas was forming and collecting in the solid waste management unit and that the pressure from this gas was causing the seepage of a tar-like NAPL to the surface. Additionally leachate is accumulating in SWMU 8 and has the potential to move laterally. In the CMS Report two corrective measure options were analyzed to address these concerns. In-place containment was the chosen remedy and the design considerations included the following criteria:

#### • <u>Repair existing cap at seep locations</u>

Areas that exhibited surface seeps of NAPL during the RFI will be investigated and addressed by either excavation of the affected area and placement of clay back into the seep, or the regrading that is to occur in order to promote positive drainage from the area may be sufficient to "re-cap" these seep areas.

• Landfill gas venting

During the RFI it was noted that landfill gas was being generated and collecting within SWMU 8. There is evidence to suggest that the gas pressure being generated was increasing the potential for the NAPL surface outbreaks. In order to alleviate the gas pressure passive vents will be installed within the lateral limits of SWMU 8.

#### • Leachate and NAPL recovery

To alleviate the potential for surface seeps and any subsurface lateral migration, leachate recovery wells will be installed within the lateral limits of SWMU 8. Leachate removal will focus on controlling migration of the accumulated liquid to maintain acceptable risk criteria.

#### • An enhanced barrier

In order to accentuate the existing low permeability soils, sheet pile will be installed below ground surface, keying into the existing upper till clay unit. The gas and leachate recovery wells will be used to maintain the liquid levels inside the barrier.

#### Additional work to be incurred on SWMU 8

Building C (AOC 5) will be removed in order to facilitate cap enhancement over SWMU 8. A replacement structure for Building C will be located elsewhere at the facility. Butz Crock (AOC 7) will be treated similarly to the noted surface seeps within SWMU 8. The crock and associated piping will be removed and backfilled with cement or other appropriate flowable fill.

Building C Heating Oil Tank (AOC 12) will be closed in place. Any liquids found within the tank will be removed and properly recycled or disposed. The tank will then be filled with cement or cement slurry to ensure that the tank does not collapse and lead to subsidence in this area. A portion or the entire tank may be removed and properly recycled or disposed if it impedes installation of the sheet pile wall.

#### 1.2 Development of Design

#### • Cap repair and enhancement

The existing cap will be repaired in the areas of NAPL surface seeps. These repairs will consist of excavating the seep area to try and identify the source. If the source can be identified an attempt to remove it will be made. After the area has been excavated soil will be placed and compacted to seal off the seep. Additional grading will be completed in accordance with the final grading plan to ensure that positive drainage off SWMU 8 is maintained.

An existing conditions survey will be completed to facilitate the final grading plan. The final grade will take the sheet pile wall into account so that positive drainage is maintained while ensuring that the sheets are appropriately covered.

#### Landfill Gas Management and Leachate Removal

The passive gas vents and leachate recovery wells are to be installed as dual purpose structures. The dual purpose structure will be designed to vent landfill gas and remove leachate from the unit from a single boring. The final recovery well/gas vent locations are based on historical information. Any revision to these locations based on conditions encountered in the field will be noted in the as-built report.

The recovery wells/gas vents will be installed in a staged manner. Recovery well/gas vents C and D will be installed first and monitored for 12 months prior to the next two extraction points being installed. The intent of installing the wells/vents in this phased manner is to determine the effectiveness of the well design, extraction equipment, and what level of extraction/venting is necessary. Should less than five extraction points accomplish the corrective action goal of eliminating surface seeps, the remaining points will not be installed.

Liquid within SWMU 8 was assessed using historical aerial photographs, historical data, and data at the time of installation from T-42S, T-54S and G-4S or their replacements. Based on the information gathered, during installation, appropriate performance objectives will be established and detailed in the operations and maintenance plan submitted with the as-built report.

The attached plan sheets contain a typical detail for the construction of the recovery well/ gas vents. This detail is intended to be flexible in the materials used for construction of the wells depending on the field conditions encountered during installation. Because the intent of the wells will be NAPL recovery, the granular backfill used to fill the annular space may be a larger pea gravel. This would allow for the NAPL to recharge faster but the intended extraction rate is slow enough that clogging would not be expected. However, field conditions may necessitate a finer granular material and if that is the case a different material will be installed. Each recovery well/gas vent will be documented in the as-built report along with any rational for alternate designs.

#### • Installation of Sheet Pile Wall

The location for the sheet pile wall was determined based on an existing conditions survey. The goal remains to install the wall as close to the lateral limits of SWMU 8 as possible. Some factors that may impact the location of the wall are the water line easement (the wall will stay outside of the City of Toledo's water line easement) and any underground structures that are encountered during installation. The final wall location will be shown on as built plans.

The sheet pile sections will be installed using a pushing method rather than pounding them into the ground as much as possible. The upper clay till should be an easy media to facilitate pushing the panels. Should obstacles (rocks) be encountered some pounding may be necessary.

#### • Demolition of Building C, the heating oil tank and Butz Crock

Building C is to be demolished. A replacement building will be constructed across York Street closer to the Cell M operations. The existing concrete slab that building C currently sits on will be left in place. The final grading of SWMU 8 takes this into account and provides for 1.5 to 2 feet of soil over the slab.

The heating oil tank (AOC 12) located on the south side of Building C will be abandoned in place. Any remaining liquid in the tank will be removed and properly recycled or disposed. The tank will then be filled with a cement, cement slurry or other appropriate flowable fill to ensure that the tank does not collapse and lead to subsidence.

Butz Crock (AOC 7) will be closed place. Any liquids found in the crock will be removed and properly disposed. The crock will then be filled with cement, cement slurry or other appropriate flowable fill to prevent subsidence in the area and to blind off any potential pathways. The flowable fill will also fill the associated piping to the degree possible.

Similarly, other any other units encountered within SWMU 8 such as the septic tank associated with AOC 4, the two waste water tanks associated with AOC 5, the second utility vault, will also be abandoned in place using the same methods.

Plan Sheet Set Sheet Pile Wall location and Details Grading Plan Recovery Wells/Gas Vent Locations and Details Surface Water Improvements





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CONTAINMENT (INTERIOR) SIDE

### <u>GENERAL NOTES</u>

- 1. ALL WIORK SHALL BE PERFORMED IN ACCORDANCE WITH APPLICABLE FEDERAL, STATE, AND LOCAL CODES AND REGULATIONS. 2. WORK POINTS WERE DEVELOPED FROM AVAILABLE SURVEY INFORMATION. THE CONTRACTOR SHALL LOCATE THE PROPOSED SHEET PILE WALL AND VERIFY ITS ALIGNMENT PRIOR TO THE START OF CONSTRUCTION. ANY DISCREPENCIES WITH THESE PLANS SHALL BE BROUGHT TO THE ATTENTION OF THE OWNER PRIOR TO THE START OF CONSTRUCTION.
- 3. ALL OBSTRUCTIONS TO THE INSTALLATION OF THE PROPOSED SHEET PILE SHALL BE REMOVED PRIOR TO SHEET PILE INSTALLATION. THE CONTRACTOR SHALL COORDINATE THE WORK WITH THE REMOVAL AND/OR RE-ROUTING OF OVERHEAD UTILITY LINES AND POLES BY THE AFFECTED UTILITY.
- 4. NO IN SITU SOIL MATERIAL SHALL BE REMOVED FROM THE SITE, OR TO ANY LOCATION OUTSIDE THE PERIMETER OF THE PROPOSED SHEET PILE WALL. REMOVED OBSTRUCTIONS AND CONSTRUCTION DEBRIS SHALL BE PLACED IN CONTAINERS PROVIDED BY OWNER FOR DISPOSAL BY OWNER, AND SHALL BE PROPERLY DISPOSED.
- 5. SPECIFICATIONS FOR SHEET PILE WITH MAY VARY FROM WHAT IS SHOWN BASED ON AVAILABILITY AT THE TIME OF PURCHASE. REGARDLESS OF THE SECTION SHAPE, SWMV 8 WILL BE CONTAINED AS INDICATED.
- 6. SHEET PILE SECTIONS ARE TO BE A MINIMUM OF 30' IN LENGTH. THIS WILL ENSURE THAT THE BOTTOM OF THE SHEETS ARE SET IN THE UNDERLYING CLAY TILL.







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## SWMU 9 NEW OIL POND



#### 1.1 Basis of Design

The purpose of this design is to develop a plan to manage the conditions identified at SWMU 9, the New Oil Pond, which require corrective measures. During the RFI it was determined that surface water was ponding on top of SWMU 9. The ponded water is infiltrating into the cap and apparently accumulating at the cap/waste interface. This accumulated water has been noted as surface seeps in various locations on SWMU 9. In the CMS Report two corrective measure options were analyzed to address the infiltration of storm water and the subsequent seepage of water accumulated under the cap material to the surface. In-place containment with a new composite cap system was the chosen remedy and the design considerations included the following criteria:

<u>The waste throughout the unit does not contain significant free liquids and/or NAPL</u>

At the time SWMU 9 was closed, the waste was sufficiently stabilized. The waste mass is not currently or expected to produce water/leachate in the future. The surface seeps and oily water accumulation noted on top of the cap is attributed to the infiltration of surface water through the cap. The infiltrated water is accumulating at the waste/cap interface and then becoming visible through the surface seeps.

<u>The waste is stable enough to support the load from the cap and equipment</u>
 The cap has not subsided since the unit was closed. This can be corroborated through historic pictures and survey information. The installation of the new composite cap will not add additional weight to the unit. The installation of a drainage layer will keep water that could act as additional driving force from collecting in the cover soils.

Much of the drainage from the cap is diverted from City of Toledo water line easement. Storm water currently accumulates in a bowl like area on the cap surface and may migrate under the cap where it is in contact with waste material at the waste/cap interface. The ponded surface water evaporates or is pumped and managed as leachate. Storm water that drains from the side slopes has not been in contact with waste and is diverted away from the City of Toledo water line easement through the trenches that border the south side of the unit. It is managed through the facility's storm water management system. The installation of an impermeable flexible membrane liner over a properly graded cap will eliminate the potential for surface water to infiltrate through a soil cap and contact the waste material. After composite cap installation any water that drains from the cap will be clean surface water and be managed though the facility's surface water management system.

#### 1.2 Development of Design

• Preparation for installation of the Composite Cap

To install the new composite cap, the existing cap will need to be removed. Any water that has accumulated at the waste/cap interface will be removed by pumping to the existing dewatering system. The leachate will be pumped into a frac tank or one of the SWMU 6 or SWMU 7 leachate tanks and properly disposed. Removal of the existing top three feet of

cap material will then be conducted to expose the new final cover subgrade. Any of the removed material that is suitable for use as frost protection will be stockpiled for use after the composite cap has been constructed. Materials that are not suitable (potentially contaminated) will be removed from SWMU 9 and disposed of in Cell M. The suitability of the subgrade material to act as a base for the cap will be determined in the field via proof rolling. Proof rolling shall be performed using a loaded haul truck with a minimum weight of 20 tons, or equivalent vehicle/equipment. An acceptable proof roll results in deformation or displacement of subgrade soils of two inches or less ( $\leq 2^n$ ). If material from this thickness needs to be removed it will be placed into the active Cell M. If the material is competent as a base for the clay cap it will be brought back up to grade as the subgrade is prepared for recompacted soil barrier construction.

#### <u>Composite Cap Construction</u>

*Recompacted Barrier Layer* – Once the subgrade is prepared, clay will be placed in 8 inch loose lifts and compacted according to ESOI's authorizing documents. The recompacted barrier layer will be installed to a final thickness of two feet.

*Flexible Membrane Liner* – A 40 mil FML will be installed over the recompacted clay barrier. The FML will be continuous across the unit and keyed into an anchor trench around the perimeter.

*Drainage Geocomposite* – In order to promote drainage of surface water off of the cap, a geocomposite will be installed on top of the FML. The geocomposite will be wrapped around perimeter collection pipes and drain pipes installed to allow the water to exit into surface water control ditches.

*Frost protection layer* – a frost protection layer will be installed over the geocomposite to insulate the recompacted barrier layer from freeze thaw cycles.

#### Final Grading

The final slopes of SWMU 9 will be graded to ensure proper drainage as described in Section I-3f of ESOI's Part B application. The unit will be graded so that water does not pond and the drainage channels direct the surface water off of the unit and into surface water control structure(s).

Plan Sheet Set Grading plan and Cap cross section details





	CORRECTIVE MEASURES IMPLEMENTATION SCHEDULE																						
ID	Task Name	Duration M-1	M1	M2	M3	M4	M5	M6	M7	M8	M9	M10	M11	M12	M13	M14 M	5 M16	M17	M18	M19	M20	M21	M22
1	Receive Ohio EPA Approval for Final Design	0 days	1/1																				
2	Corrective Measures Implementation	627 days																			•		
3	SWMU 5 (NAPL Extraction at Millard)	71 days	-																				
4	Startup/Contracting	30 days																					
5	Purchase Equipment and Delivery of System	30 days																					
6	Equipment Installation	5 days																					
7	Equipment Testing	5 days																					
8	SWMU 6 (Relocation of Waste at NSL)	60 days																					
9	Construction Sequence (See Engineering Design)	60 days																					
10	SWMU 8 (Containment of Old Oil Pond)	627 days	-																		-		
11	Startup/Contracting	45 days																					
12	Building Steel Delivery	45 days																					
13	New Building Construction	45 days																					
14	Moving	30 days																					
15	Building C Demolition	30 days																					
16	Barrier Wall Delivery	60 days																					
17	Barrier Wall Installation	40 days																					
18	Closure of Tanks and Utility Vaults	15 days																					
19	Cap Repairs and Re-grading	60 days																					
20	Installation of Leachate/NAPL and Gas Extration Wells*	400 days																					
21	SWMU 9 (New Oil Pond Cap Improvements)	308 days																					
22	Startup/Contracting	45 days																					
23	Purchase Supplies	30 days																					
24	Preparation for Composite Cap Installation	30 days																					
25	Composite Cap Construction	60 days												_									
26	Final Grading	20 days																					
	Task Summary Rolled Up Progress Deadline																						
Sched	Schedule and sequence may vary based on items such as Contractor Availability; Delivery of Split Rolled Up Task External Tasks																						
Supplies; Equipment Functionality, Weather Conditions, and Timely Reimbursement from Trust							Ro	led Un Sr	⊔ olit			Proiec	t Summary										
			Mileston	2			Ro		ilestone /	$\overline{\mathbf{a}}$		Evtorn	al Mileston			•							
*Anv S	WMU 8 recovery wells/gas vents installed following the initial evaluation of	eriod will be installed	as soon as	practical	The sche	dule allows	s for a tota	of 400 d	avs. This r	∽ mav be e×	tended to e	evaluate d	design char	nges, and	d install ad	ditional wells							
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(ix) WMU 8 Old Oil Pond

The selected remedy for WMU 8 is

- (a) Contain waste in-place by repairing cap at locations where NAPL tar seeps have been observed, installing leachate/NAPL recovery wells, installation of passive gas recovery/vents, and installation of barrier wall surrounding limits of waste.
- (b) Removal (including <u>capping of</u> floor slabs) and replacement of Building C (AOC 3) (in an alternate location), and removal <u>or stabilization and capping</u> of AOC 12, AOC 7, and AOC 5\_within the isolation barrier wall of WMU 8.
- (x) WMU 9 New Oil Pond

The selected remedy for WMU 9 is:

- (a) Upgrade Cap to a Composite Cover. This includes re-contouring of the landfill cover to provide positive drainage, and minimizing accumulation and infiltration of storm water.
- (b) Installation of recovery wells.
- (c) Excavate current cap to remove top zone of stabilized waste.
- (xi) AOC 1 Toledo Water Line

The selected remedy for AOC 1 is to reduce volume of water in trenches by removing vegetation from drainage ditches along this AOC, and re-grading and recapping the areas along waterline right-of-way to improve runoff and reduce infiltration.

(xii) AOC 5 Decontamination Building Underground Storage Tanks (UST)

The selected remedy for WMU 8 (Condition E.9(d)(ix)) also addresses AOC 5.

(xiii) AOC 7 Butz Crock — Utility Vault

The selected remedy for WMU 8 (Condition E.9(d)(ix)) also addresses AOC 7.

(xiv) AOC 12 Building "C" Heating Oil Tank

The selected remedy for WMU 8 (Condition E.9(d)(ix)) also addresses AOC 12.